
Harmonic Analysis

Physics Laboratory 3

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Abstract In this experiment, harmonic analysis of periodic signals was investigated using both frequency-selective measurements and Fourier-based spectral analysis. The properties of a precision rectifier and a band-pass filter were characterized, and the filter response was fitted with a Lorentzian model, yielding a resonance frequency of $f_0 = (95.0 \pm 0.8)$ kHz and a quality factor of $Q = 13 \pm 5$. Amplitude modulation was analyzed using three methods. The modulation depth was determined as $m = 0.611 \pm 0.005$ from the X-Y plot, $m = 0.727 \pm 0.002$ from the time-domain oscilloscope trace, and $m = 0.0092 \pm 0.0004$ from the FFT spectrum. The first two methods gave values of the same order of magnitude, whereas the FFT-based result was significantly smaller. In addition, Fourier spectra of sinusoidal and triangular signals were recorded with a digital oscilloscope. Both signals showed a fundamental frequency near 34.5 kHz, while the triangular waveform exhibited a more pronounced odd-harmonic structure. Finally, the total harmonic distortion of a distorted sinusoidal signal was found to be $\text{THD} = (1.11 \pm 0.02)\%$. Overall, the measurements were largely consistent with the theoretical expectations, except for the FFT-based determination of the modulation depth.

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Introduction

The analysis of signals in both the time and frequency domains is a fundamental tool in modern physics and electrical engineering. While signals are commonly observed as functions of time, their representation in the frequency domain often provides deeper insight into their structure, transmission properties, and interaction with linear systems. The mathematical foundation of this approach is given by Fourier analysis, which allows periodic signals to be decomposed into harmonic components and arbitrary signals to be represented by their frequency spectra [2].

In communication systems, frequency-domain analysis plays a crucial role. For efficient transmission of information via electromagnetic waves, low-frequency signals are typically shifted to higher frequency ranges. This process, known as modulation, enables wireless transmission, improves signal-to-noise ratios, and allows multiple signals to share a common transmission medium. In particular, amplitude modulation (AM) modifies the amplitude of a high-frequency carrier wave according to a lower-frequency information signal. The resulting spectrum contains the carrier frequency as well as sidebands that encode the transmitted information.

The present experiment focuses on harmonic analysis and amplitude modulation. The primary objective is to investigate the frequency spectra of various periodic signals and to compare different methods of spectral analysis. A frequency-mixing measurement technique using a modulator and a band-pass filter is employed to resolve individual frequency components. The results are compared with Fast Fourier Transform (FFT) measurements obtained from a digital oscilloscope and with numerical Fourier analysis of digitally recorded data.

Furthermore, the transfer functions of linear systems such as low-pass, high-pass, and band-pass filters are examined. Their influence on signal spectra is analyzed in terms of amplitude response, resonance behavior, and quality factor. Special attention is given to balanced amplitude modulation and the determination of the degree of modulation. Finally, the total harmonic distortion (THD) is measured as a quantitative indicator of signal purity.

This experiment, therefore, combines theoretical concepts of Fourier analysis and the frequency response of linear systems with practical measurement techniques used in signal processing and telecommunications.

Experiment

The experimental arrangement is designed to investigate amplitude modulation and to perform harmonic (frequency) analysis of periodic signals. A schematic overview of the setup is shown in the laboratory manual. The system consists of a signal source, a modulator, a band-pass filter, a rectifier, measurement instruments, and a computer for data acquisition.

Signal Sources

Two function generators are used. One generator provides the high-frequency carrier signal f_C , while the second generator produces the low-frequency modulation signal f_M . Depending on the measurement task, different waveforms (sinusoidal, rectangular, triangular, or pulse signals) can be selected.

For frequency-selective measurements, the carrier frequency can be varied linearly in time by means of a ramp generator. The ramp voltage controls a voltage-controlled oscillator (VCO), allowing a continuous scan of the frequency range of interest.

Modulator

The modulation is performed using an analogue multiplier. The device multiplies the carrier signal with the modulation signal, resulting in an amplitude-modulated output signal. The modulation depth can be adjusted via offset voltages, which allow operation in standard amplitude modulation or in balanced modulation (carrier suppression).

The amplification factor of the modulator is approximately constant within its linear operating range. Care must be taken to avoid overmodulation or saturation effects.

Band-Pass Filter

After modulation, the signal is fed into a third-order band-pass filter with a fixed resonance frequency of approximately 90 kHz. The filter exhibits a high quality factor ($Q \approx 100$), providing strong frequency selectivity.

By sweeping the carrier frequency, individual spectral components of the modulation signal are shifted into the resonance range of the filter. Only frequency components within the narrow bandwidth of the filter are transmitted with significant amplitude. This enables selective measurement of single harmonics.

Rectifier and Amplitude Measurement

The filtered signal is passed through a precision rectifier. The rectifier converts the alternating signal into a proportional DC voltage, allowing accurate amplitude measurements.

Depending on the selected amplification factor, small signals can be measured with increased sensitivity. The output voltage of the rectifier is recorded either with multimeters or displayed on the oscilloscope.

Oscilloscope and Data Acquisition

Both an analogue and a digital oscilloscope are used. The analogue oscilloscope enables direct visualization of time-domain signals and x-y plots (e.g. for the modulation trapezoid). The digital oscilloscope allows Fast Fourier Transform (FFT) analysis and digital storage of measured data.

The recorded data can be transferred to a computer for numerical Fourier analysis and comparison with theoretical Fourier coefficients.

Measurement Strategy

The experiment proceeds by first characterizing the individual components (rectifier and filter), followed by measurements of amplitude-modulated signals. Subsequently, Fourier spectra of various periodic signals are recorded using three different methods:

- frequency-selective measurement with the band-pass filter,
- FFT analysis using the digital oscilloscope,
- numerical Fourier transformation of stored signal data.

Finally, the total harmonic distortion (THD) of selected signals is determined from their measured spectra.

Results

Characteristics of the Rectifier (Raw Data)

Table 1: Rectifier raw data for the K_1 and K_{10} settings.

K_1 setting		K_{10} setting	
V_{in} (V)	V_{out} (V)	V_{in} (V)	V_{out} (V)
4.71	4.11	4.71	41.2
5.03	4.40	5.07	44.5
7.43	6.43	7.41	64.5
9.78	8.53	9.94	86.5
12.10	10.60	12.10	105
14.70	12.80	14.60	128
18.30	16.00	15.30	135
21.40	18.80	15.80	139
23.40	20.30	16.00	141
26.00	22.60	16.40	141
30.20	26.80	18.50	141
37.40	33.60	21.30	141
42.20	37.90	23.30	141
46.80	42.20	30.20	141
50.40	45.40	40.20	141
55.50	49.60	50.30	141
61.20	54.90	74.50	141
65.30	58.70		
70.50	63.40		
74.50	67.00		

Characteristics of the Filter (Raw Data)

Table 2: Raw measurement data used for the characterization of the band-pass filter.

(a) Band-pass filter raw data for linearity test (measured close to resonance).

V_{in} (V)	V_{out} (V)
4.67	2.28
5.05	2.51
7.56	3.60
10.00	4.75
15.10	7.26
19.90	9.51
25.10	12.00
30.00	14.50
35.10	16.90
39.90	19.20
45.00	21.60
50.20	23.90
55.10	26.20
60.10	28.70
65.10	31.00
68.90	32.80
73.90	35.10

(b) Band-pass filter resonance curve raw data ($V_{\text{in}} = 3.74$ V constant).

f (kHz)	V_{out} (V)
59.8	0.511
70.5	0.522
80.6	0.526
85.1	0.527
88.9	0.532
91.8	0.545
93.8	0.552
95.9	0.563
98.2	0.542
100.0	0.530
105.1	0.523
110.2	0.522

Balanced Modulation (Raw Data)

Two oscilloscope recordings of the amplitude-modulated signal were used for the later determination of the modulation depth: an X–Y plot of the signal and a conventional time-domain oscilloscope trace (KO display). In both cases, the relevant vertical heights were measured directly from the screenshots using the *Screen Ruler* utility from Microsoft PowerToys at a zoom level of 400%.

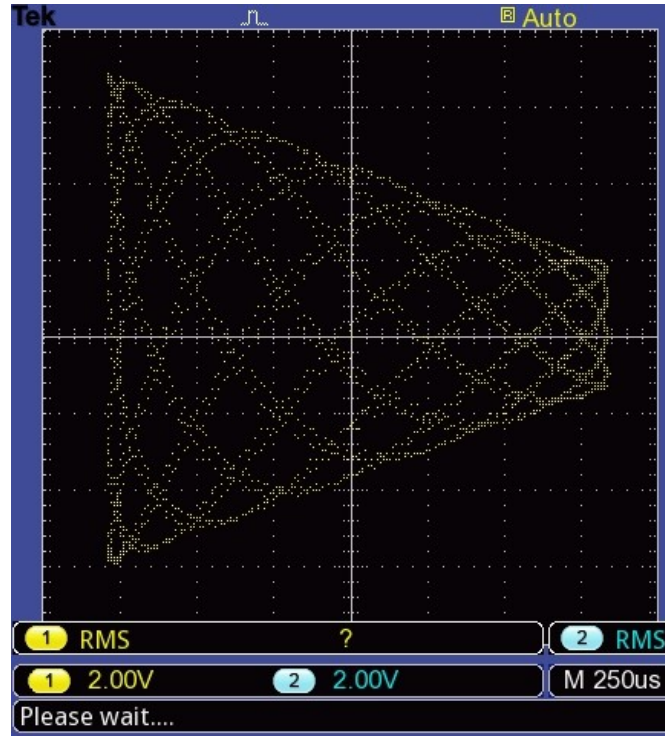


Figure 1: X–Y plot of the amplitude-modulated signal showing the characteristic trapezoidal pattern. The horizontal axis corresponds to the modulating signal, while the vertical axis corresponds to the AM signal. The maximum and minimum vertical extensions of the trapezoid were used for the determination of the modulation depth.

For the X–Y method, the measured vertical heights of the trapezoid were

$$H_{\max} = 1315 \text{ px}, \quad H_{\min} = 318 \text{ px}.$$

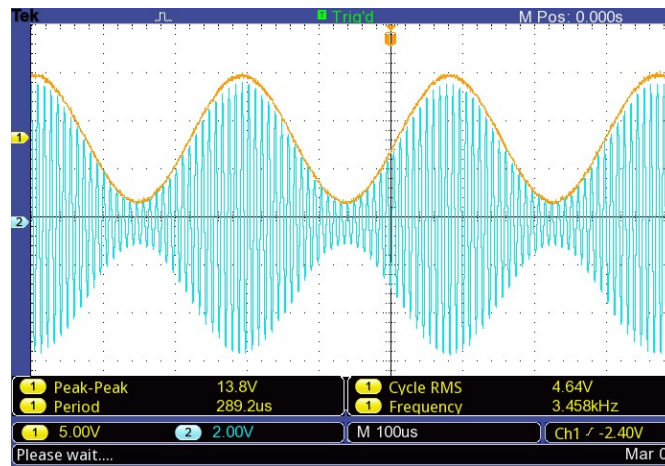


Figure 2: Time-domain oscilloscope trace of the amplitude-modulated signal (KO display). The maximum and minimum vertical signal heights, $H_{\max}$ and $H_{\min}$, were determined from the envelope and used for the time-domain evaluation of the modulation depth.

For the time-domain method, three repeated measurements were taken from the envelope. The measured values were

$$H_{\max} = (1135, 1136, 1130) \text{ px}, \quad H_{\min} = (179, 177, 182) \text{ px}.$$

Finding Fourier Spectra (Extracted Peak Values)

Sinusoidal signal (Top peaks from FFT export)

Table 3: Extracted dominant spectral peaks from `SinusoidalFFT.CSV`.

Frequency (Hz)	Amplitude (dB)
34 524.94	−6.59
103 574.81	−11.79
89 271.62	−21.39
92 724.12	−34.99
95 683.40	−36.59
84 339.49	−40.99
86 805.55	−42.59
82 859.85	−42.99
78 914.14	−44.99
73 982.01	−45.79

Triangular signal (Top peaks from FFT export)

Table 4: Extracted dominant spectral peaks from `TriangularFFT.CSV`.

Frequency (Hz)	Amplitude (dB)
34 524.94	16.21
103 574.81	−3.39
310 231.22	−22.19
448 330.96	−28.59
492 720.17	−29.79
423 177.08	−30.99
354 620.42	−32.59
69 049.87	−32.99
138 099.75	−32.99
78 420.93	−36.19

Total Harmonic Distortion (Raw Peak Values)

The amplitudes of the dominant harmonic components were obtained from the FFT spectrum measured with the oscilloscope. These peak values serve as the raw data for the later evaluation of the total harmonic distortion (THD).

Table 5: Measured amplitudes of the first harmonic components extracted from the FFT spectrum and used for the THD calculation.

Harmonic index n	Amplitude (dB)
1	28.2
2	-12.5
3	-16.1

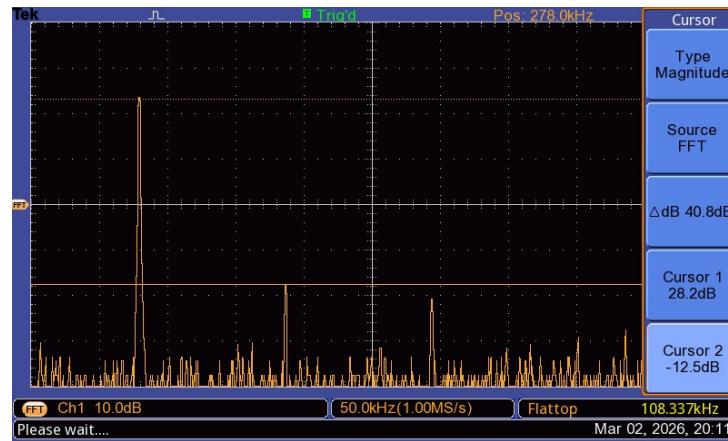


Figure 3: FFT spectrum of the measured signal showing the fundamental component and higher harmonic peaks used for the determination of the total harmonic distortion.

Data Analysis

Characteristics of the Rectifier

The transmission characteristics of the precision rectifier were measured for both gain settings K_1 and K_{10} . In each case, a linear model constrained through the origin was used:

$$V_{\text{out}} = K_i V_{\text{in}}. \quad (1)$$

For the K_1 setting, using all measured points, the fit yielded

$$K_1 = 0.8962 \pm 0.0018 \quad (2)$$

For the K_{10} setting, linear behavior was observed only up to $V_{\text{in}} \leq 16.0$ V. Restricting the fit to this region gave

$$K_{10} = 8.774 \pm 0.018. \quad (3)$$

Above $V_{\text{in}} \approx 16$ V, the output voltage saturated at approximately $V_{\text{out}} \approx 141$ V, indicating the limit of the linear operating range.

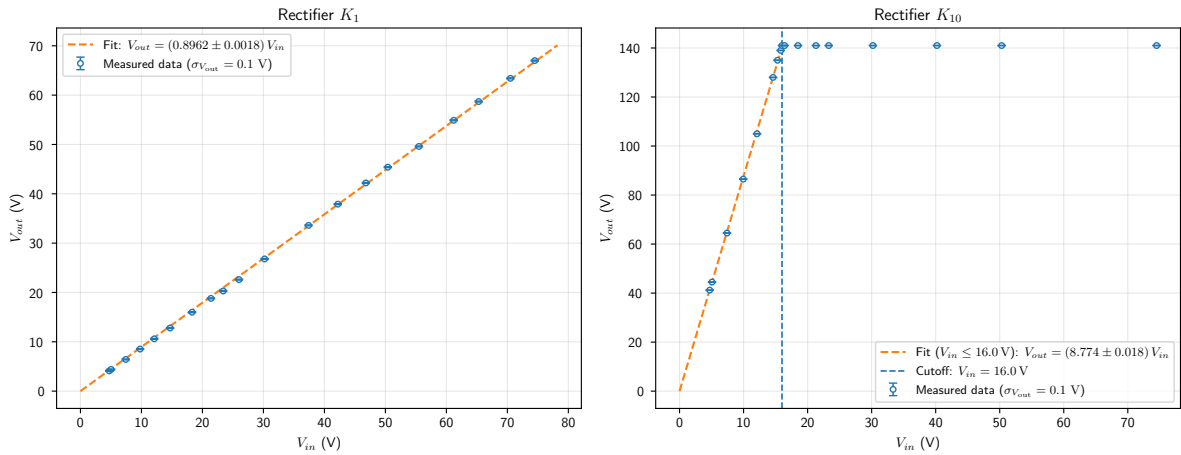


Figure 4: Measured transfer characteristics of the rectifier for the K_1 and K_{10} settings. The dashed lines indicate the linear fits to the data. For the K_{10} configuration the output voltage saturates above $V_{\text{in}} \approx 16$ V.

Characteristics of the Filter (Linearity)

The linear operating range of the band-pass filter was investigated by measuring V_{out} as a function of V_{in} close to resonance. A linear regression yielded

$$V_{\text{out}} = (0.4752 \pm 0.0009) V_{\text{in}} + (0.10 \pm 0.04) \text{ V}, \quad (4)$$

with a coefficient of determination

$$R^2 = 0.99994. \quad (5)$$

confirming highly linear behavior in the investigated amplitude range.

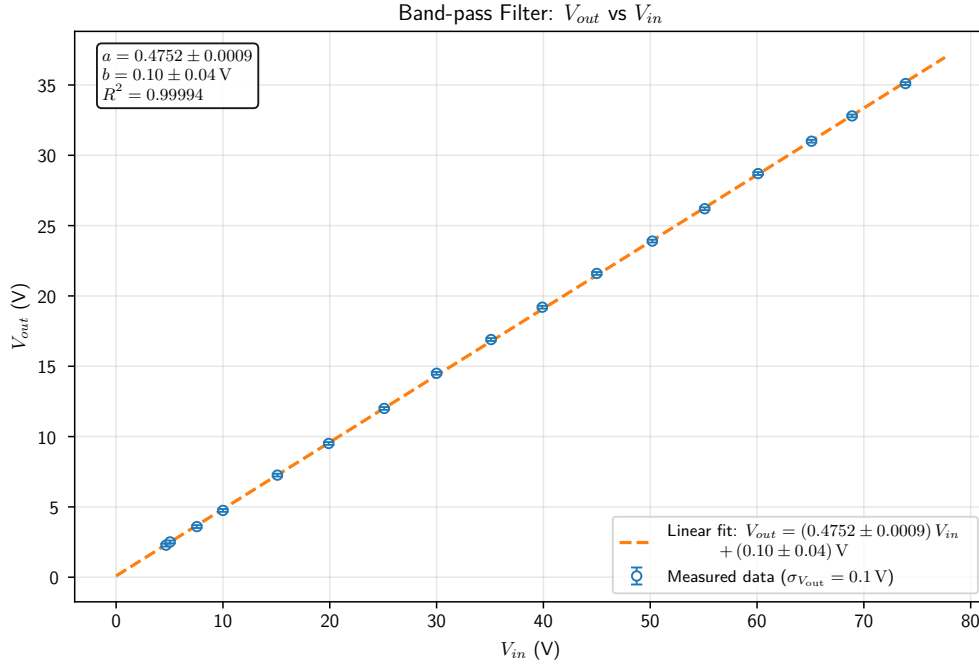


Figure 5: Measured output voltage V_{out} as a function of the input voltage V_{in} for the band-pass filter at resonance. The dashed line represents the linear regression used to determine the filter gain.

In addition, the gain

$$G = \frac{V_{out}}{V_{in}} \quad (6)$$

was evaluated as a function of V_{in} , showing an approximately constant value around $G = 0.477 \pm 0.001$, within measurement uncertainties.

Characteristics of the Filter (Resonance Curve)

The frequency response of the band-pass filter was investigated for a constant input voltage $V_{in} = 3.74$ V. The gain was defined as

$$G(f) = \frac{V_{out}(f)}{V_{in}}. \quad (7)$$

Before analyzing the resonance behavior, the ratio V_{out}/V_{in} was examined as a function of the input voltage. Figure 6 shows that the gain remains approximately constant within the measurement uncertainties over the investigated voltage range. This indicates that the filter operates linearly under the chosen excitation conditions.

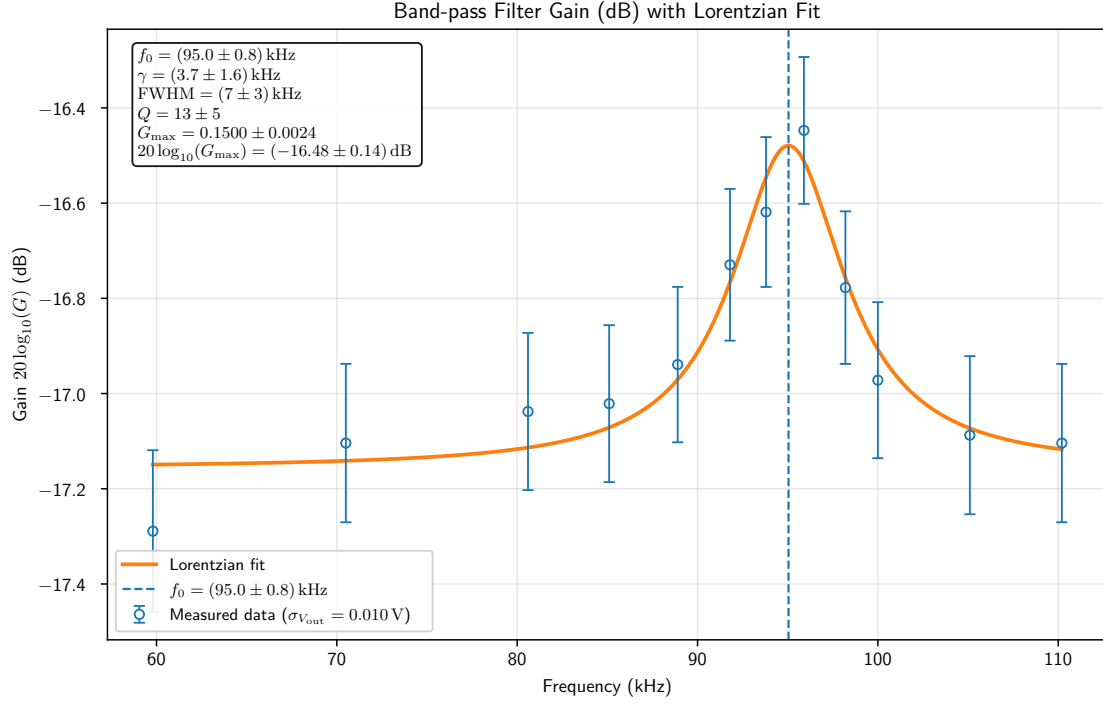


Figure 6: Measured gain $20\log_{10}(G)$ of the band-pass filter as a function of the excitation frequency f . The data points represent the measured values with their propagated uncertainties. The solid curve shows the Lorentzian fit used to determine the resonance frequency f_0 and the bandwidth of the filter. The dashed vertical line indicates the fitted resonance frequency.

To determine the resonance properties of the band-pass filter, the gain was then measured as a function of frequency. The resulting resonance curve was fitted with a Lorentzian model,

$$G(f) = y_0 + \frac{A}{1 + \left(\frac{f-f_0}{\gamma}\right)^2}, \quad (8)$$

where f_0 is the resonance frequency and γ is the half-width at half-maximum (HWHM). Figure 7 shows the measured gain in decibels together with the fitted Lorentzian function.

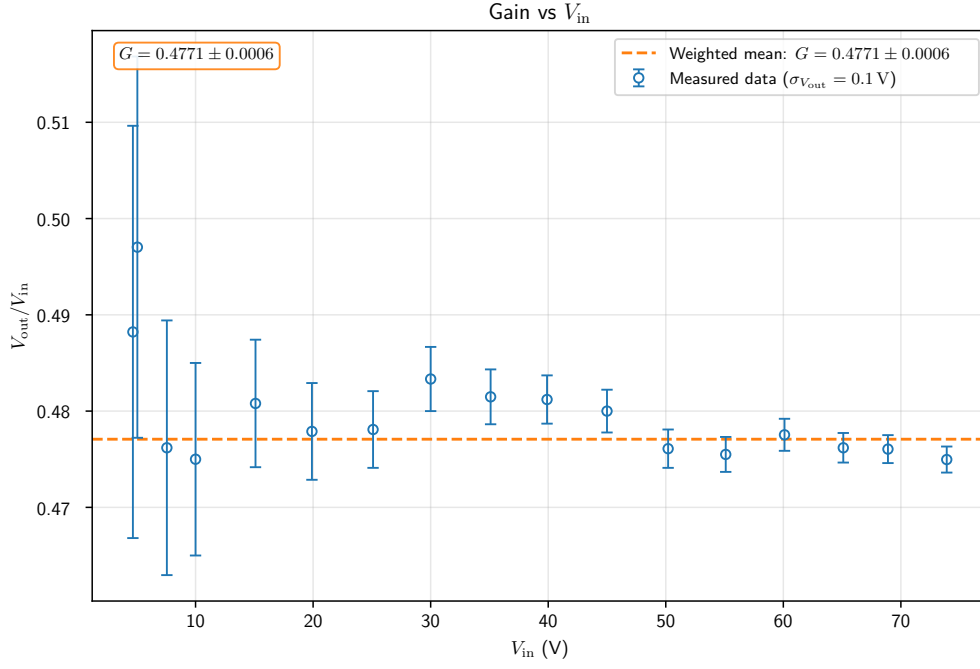


Figure 7: Measured gain $G = V_{\text{out}}/V_{\text{in}}$ as a function of the input voltage V_{in} . The error bars represent the propagated uncertainty resulting from the measurement uncertainty of V_{out} .

The fit yielded a resonance frequency of

$$f_0 = (95.0 \pm 0.8) \text{ kHz}, \quad (9)$$

and a half-width at half-maximum of

$$\gamma = (3.7 \pm 1.6) \text{ kHz}. \quad (10)$$

From this, the full width at half maximum was obtained as

$$\text{FWHM} = 2\gamma = (7.4 \pm 3.2) \text{ kHz}, \quad (11)$$

which gives the quality factor

$$Q = \frac{f_0}{\text{FWHM}} = 13 \pm 5. \quad (12)$$

The maximum gain of the filter was found to be

$$G_{\text{max}} = 0.1500 \pm 0.0024, \quad (13)$$

$$20 \log_{10}(G_{\text{max}}) = (-16.48 \pm 0.14) \text{ dB}. \quad (14)$$

Influence of f_M , Modulation Depth m , and Offset OS

Change of Modulation Frequency f_M

Changing the modulation frequency f_M affects the temporal behavior of the envelope and the spacing of the spectral components. Increasing f_M results in a faster oscillation of the envelope in the time domain. In the frequency spectrum, the sidebands appear at

$$f = f_C \pm f_M, \quad (15)$$

where f_C is the carrier frequency. Therefore, increasing f_M increases the distance between the carrier peak and the sidebands, while decreasing f_M reduces this spacing.

Change of Modulation Depth m

Adjusting the **MOD** control changes the modulation depth m and therefore the maximum and minimum values of the envelope. A larger modulation depth increases the difference between envelope maximum and minimum, resulting in a stronger amplitude variation. In the frequency spectrum, increasing m increases the amplitude of the sidebands relative to the carrier.

Change of Offset OS

Changing the **OFFSET** modifies the DC component of the modulating signal and affects the symmetry and overall shape of the envelope. Depending on the offset value, the envelope may appear shifted or distorted. If the offset is adjusted such that the carrier component is suppressed, the system approaches balanced modulation, where the carrier peak in the frequency spectrum disappears.

Determination of the Modulation Depth

The modulation depth m of the amplitude-modulated signal was determined using three independent methods: from the X-Y plot, from the time-domain oscilloscope trace (KO display), and from the frequency spectrum. Ideally, the modulation depth should be determined from three independent data sets for each of the three methods. However, only one recorded data set was available for each method in the present experiment, so the following analysis is based on one data set per method. For the first two methods, the relevant vertical dimensions were measured directly from screenshots in pixel units using the *Screen Ruler* utility from Microsoft PowerToys.

In the following, the modulation depth is defined as

$$m = \frac{A_{\max} - A_{\min}}{A_{\max} + A_{\min}}, \quad (16)$$

where $A_{\max}$ and $A_{\min}$ denote the maximum and minimum envelope amplitudes, respectively. In practice, the full vertical signal heights $H_{\max}$ and $H_{\min}$ were measured instead of the amplitudes themselves. Since

$$A_{\max} = \frac{H_{\max}}{2}, \quad A_{\min} = \frac{H_{\min}}{2}, \quad (17)$$

the same expression can equivalently be written as

$$m = \frac{H_{\max} - H_{\min}}{H_{\max} + H_{\min}}. \quad (18)$$

Thus, the quantities A and H are used interchangeably in the following wherever only their ratio enters the calculation of m .

Determination of the Modulation Depth via X–Y Plot

In X–Y mode, the modulating signal was connected to the horizontal axis and the AM signal to the vertical axis, resulting in the characteristic trapezoidal pattern. The maximum and minimum vertical extensions of the trapezoid were measured directly from the screenshot fig. 1. The measured values were

$$H_{\max} = (1315 \pm 5) \text{ px}, \quad H_{\min} = (318 \pm 5) \text{ px}.$$

A conservative uncertainty of 5 px was assigned to both values to account for the finite line thickness, limited image sharpness, and the manual placement of the measurement markers. Using eq. 18 the modulation depth was found to be

$$m = 0.611 \pm 0.005. \quad (19)$$

Determination of the Modulation Depth via Time-Domain Oscilloscope Trace

In the normal oscilloscope time-domain display (KO), the envelope of the amplitude-modulated signal was used to determine the maximum and minimum vertical signal heights. Three repeated measurements were taken from the screenshot fig. 2, yielding

$$H_{\max} = (1135, 1136, 1130) \text{ px}, \quad H_{\min} = (179, 177, 182) \text{ px}.$$

From these values, the mean heights and their uncertainties were obtained as

$$H_{\max} = (1133.7 \pm 1.9) \text{ px}, \quad H_{\min} = (179.3 \pm 1.5) \text{ px}.$$

Using eq. 18 the modulation depth was determined to be

$$m = 0.7268 \pm 0.0019. \quad (20)$$

Determination of the Modulation Depth via Frequency Spectrum

In the FFT spectrum of the amplitude-modulated signal, the carrier peak and the two sidebands were identified manually from the recorded spectrum. The selected peak frequencies were

$$f_{\text{LSB}} = 705.3 \text{ Hz}, \quad f_C = 754.6 \text{ Hz}, \quad f_{\text{USB}} = 803.9 \text{ Hz}.$$

The corresponding amplitudes read from the FFT trace were

$$A_{\text{LSB}} = -32.95 \text{ dB}, \quad A_C = 13.45 \text{ dB}, \quad A_{\text{USB}} = -33.75 \text{ dB}.$$

Since the FFT amplitudes were given in decibels, they were converted to linear amplitudes according to

$$A_{\text{lin}} = 10^{A_{\text{dB}}/20}. \quad (21)$$

For an amplitude-modulated signal with carrier, the sideband amplitudes satisfy

$$A_{\text{LSB}} = A_{\text{USB}} = \frac{m}{2} A_C.$$

Thus, the modulation depth can be obtained from the spectrum using

$$m = \frac{A_{\text{LSB}} + A_{\text{USB}}}{A_C}. \quad (22)$$

Using Eq. (21) and Eq. (22), the modulation depth was found to be

$$m = 0.0092 \pm 0.0004. \quad (23)$$

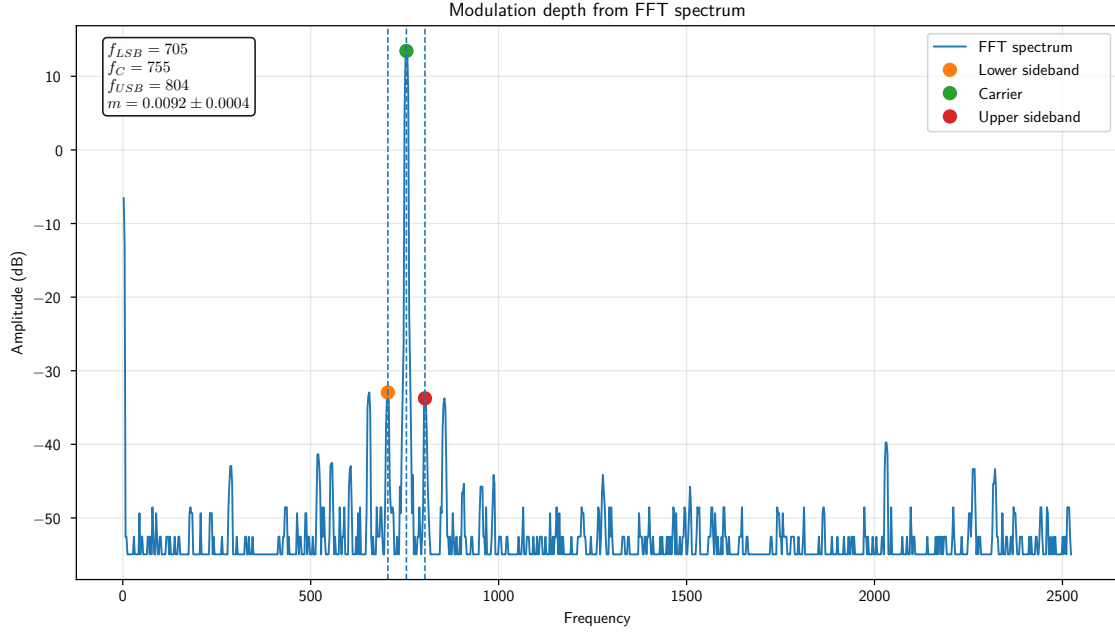


Figure 8: FFT spectrum of the amplitude-modulated signal. The carrier peak and the two sidebands used for the spectral determination of the modulation depth are marked.

Comparison of the Three Methods

For clarity, the modulation depths obtained with the three independent methods are summarized in Table 6. The X–Y plot and the time-domain oscilloscope trace yield values of the same order of magnitude, whereas the value obtained from the FFT spectrum is significantly smaller.

Table 6: Comparison of the modulation depth determined by the three evaluation methods.

Method	Modulation depth m
X–Y plot	0.611 ± 0.005
Time-domain oscilloscope trace (KO)	0.727 ± 0.002
Frequency spectrum (FFT)	0.0092 ± 0.0004

Finding Fourier Spectra

The Fourier spectra of different periodic input signals were analyzed using the FFT function of the digital oscilloscope. The exported spectra were evaluated by identifying the dominant spectral peaks and comparing their positions with the expected harmonic frequencies.

For both the sinusoidal and triangular signals, the strongest component was found near

$$f_1 \approx 34.5 \text{ kHz}, \quad (24)$$

which is identified as the fundamental frequency of the excitation signal. Additional peaks at higher frequencies were interpreted as harmonic components.

Sinusoidal Signal

For the sinusoidal signal, the dominant spectral peak was found at

$$f_1 = (34.5 \pm 0.3) \text{ kHz}, \quad A_1 = (-6.6 \pm 0.4) \text{ dB}. \quad (25)$$

A further pronounced component appeared at

$$f_3 = (103.6 \pm 0.3) \text{ kHz}, \quad A_3 = (-11.8 \pm 0.6) \text{ dB}. \quad (26)$$

Since

$$103.6 \text{ kHz} \approx 3 \cdot 34.5 \text{ kHz}, \quad (27)$$

this peak can be assigned to the third harmonic. Ideally, a purely sinusoidal signal should contain only the fundamental frequency. The appearance of higher-frequency components therefore indicates deviations from an ideal sine wave, for example due to signal distortion, limited generator quality, or instrumental effects of the measurement chain.

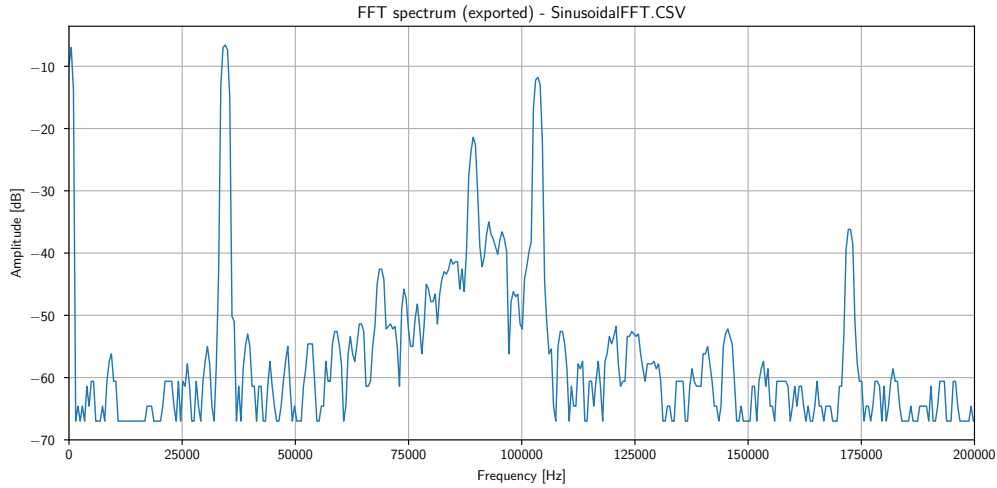


Figure 9: FFT spectrum of the sinusoidal signal. The dominant peak corresponds to the fundamental frequency at approximately 34.5 kHz, while a smaller peak is visible near the third harmonic at approximately 103.6 kHz.

Triangular Signal

For the triangular signal, the fundamental component was observed at

$$f_1 = (34.5 \pm 0.3) \text{ kHz}, \quad A_1 = (16.2 \pm 0.4) \text{ dB}. \quad (28)$$

A pronounced higher harmonic was found at

$$f_3 = (103.6 \pm 0.3) \text{ kHz}, \quad A_3 = (-3.4 \pm 0.6) \text{ dB}. \quad (29)$$

Again,

$$103.6 \text{ kHz} \approx 3 \cdot 34.5 \text{ kHz}, \quad (30)$$

so this component is identified as the third harmonic. This is consistent with the Fourier series of a triangular waveform, which contains predominantly odd harmonics, while the amplitudes decrease strongly with increasing harmonic order. Compared with the sinusoidal signal, the triangular signal therefore exhibits a richer harmonic structure.

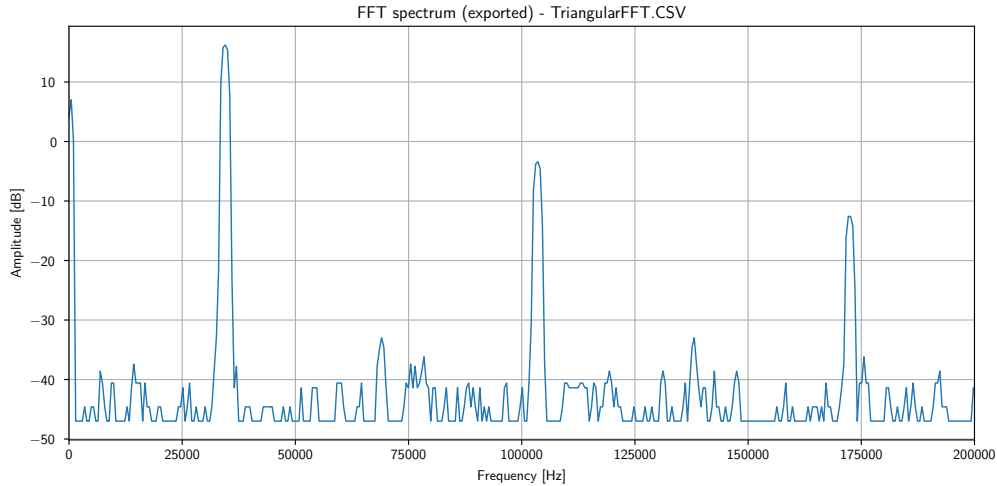


Figure 10: FFT spectrum of the triangular signal. Besides the fundamental frequency at approximately 34.5 kHz, a clear third harmonic near 103.6 kHz is visible, as expected for a triangular waveform.

Comparison of the Spectra

The extracted dominant spectral components are summarized in Table 7. In both cases, the fundamental frequency is located at approximately 34.5 kHz. For the sinusoidal signal, the spectrum is dominated by the fundamental component, with only a comparatively weak higher harmonic. For the triangular signal, higher harmonics are more clearly visible, in agreement with the expected Fourier decomposition of a non-sinusoidal periodic waveform.

Table 7: Dominant spectral peaks extracted from the FFT spectra.

Signal	Frequency (kHz)	Amplitude (dB)
Sinusoidal	34.5 ± 0.3	-6.6 ± 0.4
Sinusoidal	103.6 ± 0.3	-11.8 ± 0.6
Triangular	34.5 ± 0.3	16.2 ± 0.4
Triangular	103.6 ± 0.3	-3.4 ± 0.6

Overall, the FFT analysis confirms the expected spectral behavior of the investigated signals. The sinusoidal waveform is characterized mainly by its fundamental frequency, whereas the triangular waveform contains pronounced odd harmonics. Small additional peaks and fluctuations in the spectra can be attributed to measurement noise, the finite frequency resolution of the FFT, and non-ideal signal generation.

Determining the Total Harmonic Distortion

To quantify the distortion of a low-quality sinusoidal signal, the total harmonic distortion (THD) was determined from the measured Fourier spectrum. The FFT spectrum recorded on the oscilloscope is shown in Figure 11.

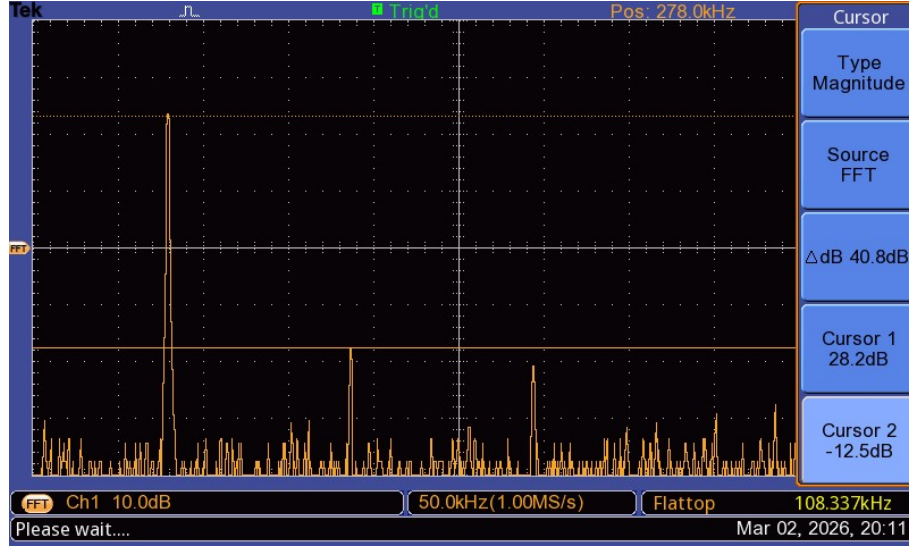


Figure 11: FFT spectrum of a distorted sinusoidal signal measured with the oscilloscope. The cursor positions mark the amplitudes used to determine the harmonic distortion.

From the spectrum, the three dominant components were identified as:

$$A_1 = (28.2 \pm 0.1) \text{ dB}, \quad A_2 = (-12.5 \pm 0.1) \text{ dB}, \quad A_3 = (-16.1 \pm 0.1) \text{ dB}. \quad (31)$$

Here A_1 represents the amplitude of the fundamental frequency, while A_2 and A_3 correspond to higher harmonic components.

Since the FFT amplitudes are given in decibel units, they were first converted to linear amplitudes using

$$A_{\text{lin}} = 10^{A_{\text{dB}}/20}. \quad (32)$$

The total harmonic distortion (THD) is defined as the ratio of the root-mean-square amplitude of the harmonic components to the amplitude of the fundamental frequency:

$$\text{THD} = \sqrt{\frac{A_2^2 + A_3^2}{A_1^2}}. \quad (33)$$

Using the measured amplitudes, the distortion was calculated as

$$\text{THD} \approx 0.0111 \pm 0.0002 = (1.11 \pm 0.02)\%. \quad (34)$$

This result indicates that the investigated signal contains a small but measurable contribution from higher harmonics. Ideally, a perfect sinusoidal signal would exhibit only the fundamental frequency in the Fourier spectrum, corresponding to a THD of zero. The observed distortion can be attributed to imperfections of the signal generator and measurement electronics.

Discussion

The performed measurements allow a comprehensive investigation of harmonic analysis and amplitude modulation using both frequency-selective techniques and Fourier-based spectral analysis. Overall, the experimental results show good agreement with the theoretical expectations for linear systems, modulation behavior, and Fourier spectra of periodic signals.

The characteristics of the precision rectifier were first examined for the gain settings K_1 and K_{10} . For the lower gain setting, the measured data followed a linear relation between V_{out} and V_{in} , yielding a proportionality factor of $K_1 = 0.8962 \pm 0.0018$. This confirms that the rectifier operates approximately linearly in this regime. For the higher gain setting, linear behavior was observed only for input voltages up to approximately $V_{\text{in}} \leq 16$ V. Beyond this limit, the output voltage saturated at about 141 V, indicating the maximum output range of the rectifier electronics. Such saturation effects are expected in practical circuits due to limited supply voltages and amplifier constraints.

The linearity of the band-pass filter was investigated close to its resonance frequency. The measured relation between V_{out} and V_{in} showed excellent linear behavior with a regression coefficient $R^2 = 0.99994$. This confirms that the filter operated within its linear regime for the investigated amplitude range. The measured gain of approximately $G = 0.477 \pm 0.001$ remained nearly constant over the investigated voltage interval, indicating that no significant nonlinear effects or signal distortions occurred during these measurements.

The resonance behavior of the band-pass filter was analyzed by measuring the gain as a function of frequency. A Lorentzian function provided a good description of the measured resonance curve. The fit yielded a resonance frequency of $f_0 = (95.0 \pm 0.8)$ kHz and a full width at half maximum of $\text{FWHM} = (7.4 \pm 3.2)$ kHz, corresponding to a quality factor of $Q \approx 13 \pm 5$. The comparatively small quality factor compared to the value suggested in the laboratory manual can be attributed to additional damping in the circuit, non-ideal electronic components, and the finite bandwidth of the measurement electronics [1]. While the laboratory description suggests a considerably higher theoretical quality factor, the experimentally observed value is smaller. This discrepancy can be attributed to several factors, including additional damping in the electronic components, non-ideal filter elements, and measurement uncertainties in the amplitude determination. In practical analog filters, such deviations from ideal behavior are common due to resistive losses and finite component tolerances.

The behavior of amplitude modulation was investigated using three independent methods for determining the modulation depth: the X–Y plot, the time-domain oscilloscope trace (KO display), and the frequency spectrum. In X–Y mode, the oscilloscope showed the characteristic trapezoidal pattern of an amplitude-modulated signal, from which a modulation depth of $m = 0.611 \pm 0.005$ was obtained. The evaluation of the time-domain envelope yielded $m = 0.727 \pm 0.002$, which is of the same order of magnitude, although somewhat larger than the value obtained from the X–Y plot. Both results indicate moderate modulation, for which the envelope remains clearly visible and no overmodulation occurs.

In contrast, the modulation depth obtained from the FFT spectrum, $m = 0.0092 \pm 0.0004$, is significantly smaller than the values determined by the other two methods and is therefore not consistent with them. This strongly suggests that the spectral evaluation is affected by systematic errors or by an incorrect identification of the relevant sideband amplitudes. Possible reasons include the limited frequency resolution of the recorded FFT trace, insufficient separation of the sidebands from nearby spectral peaks, inaccuracies in the manual peak selection, or additional spectral components and noise. The FFT-based result should therefore be treated with caution.

The Fourier spectra obtained from the digital oscilloscope further illustrate the spectral composition of periodic signals. For the sinusoidal waveform, the spectrum was dominated by a strong fundamental component at approximately (34.5 ± 0.3) kHz. A smaller peak at about (103.6 ± 0.3) kHz corresponds to the third harmonic. Ideally, a perfect sinusoidal signal should contain only the fundamental frequency; therefore, the presence of higher harmonics indicates slight distortions of the generated waveform or measurement artifacts in the signal chain.

For the triangular signal, the spectrum contained a more pronounced harmonic structure. In addition to the fundamental frequency, a clear third harmonic was observed, which is consistent with the Fourier series representation of a triangular waveform. Such signals are known to contain only odd harmonics, with amplitudes decreasing rapidly with increasing harmonic order. The experimental spectra, therefore, qualitatively confirm the theoretical harmonic content of triangular signals.

Finally, the total harmonic distortion of a deliberately degraded sinusoidal signal was determined from its Fourier spectrum. The calculated value of $\text{THD} \approx (1.11 \pm 0.02)\%$ indicates that only a small fraction of the signal power is contained in higher harmonics. Although this distortion is clearly measurable, the signal can still be considered relatively pure. The remaining harmonic components are most likely caused by imperfections of the

signal generator, nonlinearities in the electronic components, and the finite resolution of the FFT measurement.

Overall, the experiment demonstrates the close connection between time-domain signals and their frequency-domain representation. The combination of frequency-selective filtering, FFT analysis, and numerical evaluation provides consistent results and confirms the theoretical predictions of Fourier analysis and linear system response.

Conclusion

In this experiment, harmonic analysis of periodic signals was investigated using both frequency-selective measurements and Fourier-based spectral analysis. The characteristics of the precision rectifier and of the band-pass filter were successfully determined, showing linear behavior within the expected operating ranges. For the filter, the resonance frequency was found to be $f_0 = (95.0 \pm 0.8)$ kHz, with a corresponding full width at half maximum of $\text{FWHM} = (7.4 \pm 3.2)$ kHz and a quality factor of $Q = 13 \pm 5$.

The behavior of amplitude modulation was examined using three independent methods for determining the modulation depth. The X-Y plot yielded $m = 0.611 \pm 0.005$, while the time-domain oscilloscope trace gave $m = 0.727 \pm 0.002$. These two values are of the same order of magnitude and both indicate moderate modulation without overmodulation. In contrast, the value obtained from the FFT spectrum, $m = 0.0092 \pm 0.0004$, was significantly smaller and therefore not consistent with the other two methods. This discrepancy suggests that the spectral determination was affected by systematic uncertainties, most likely related to the identification of the relevant sideband amplitudes and the limited resolution of the available FFT trace.

Furthermore, the Fourier spectra of sinusoidal and triangular signals were analyzed using the FFT function of the digital oscilloscope. The measured spectra confirmed the expected harmonic structure of the signals: the sinusoidal waveform was dominated by its fundamental frequency, while the triangular waveform exhibited a more pronounced odd-harmonic content, including a clear third harmonic. Finally, the total harmonic distortion of a distorted sinusoidal signal was determined to be $\text{THD} = (1.11 \pm 0.02)\%$, indicating a small but measurable contribution from higher harmonics.

Overall, the experiment demonstrates the close connection between time-domain signals and their frequency-domain representation. With the exception of the FFT-based modulation-depth determination, the measurements are consistent with the theoretical expectations of Fourier analysis, amplitude modulation, and linear system response.

Appendix

Acknowledgments

I would like to thank my teaching assistant, Takahiro Uto, for his supervision and support during the experiment. His guidance and explanations were very helpful throughout the laboratory work and the interpretation of the results.

AI Usage Declaration

This report was prepared with assistance from ChatGPT (OpenAI) for language polishing, formatting suggestions, and for helping to develop, debug, and correct the syntax of the Python code. The AI was not used to generate raw data, to select results, or to determine the final conclusions. All scientific content (methods, calculations, results, and interpretation) was critically reviewed and validated by the authors. The authors take full responsibility for the accuracy of the analysis and for any remaining errors. No confidential or personal data were provided to the AI system during the preparation of this report.

References

- [1] Paul Horowitz and Winfield Hill. *The Art of Electronics*. 3rd ed. Cambridge University Press, 2015.
- [2] Reiner Mühle. *Harmonic Analysis*. Advanced Physics Laboratory Manual. Translation by Colin v. Negenborn (2010); laboratory manual for the Advanced Physics Laboratory, ETH Zürich; accessed via Moodle. ETH Zürich, Department of Physics, 2001.

Python Code

```

1  import os
2  import glob
3  import re
4
5  import numpy as np
6  import pandas as pd
7  import matplotlib.pyplot as plt
8
9  from scipy.stats import linregress
10 from scipy.optimize import curve_fit
11
12 from scipy.signal import find_peaks
13
14
15 # -----
16 # 5.1 Characteristics of the Rectifier
17 # -----
18
19 # K1 data
20 V_in_k1 = np.array([
21     4.71, 5.03, 7.43, 9.78, 12.1, 14.7, 18.3, 21.4, 23.4, 26.0,
22     30.2, 37.4, 42.2, 46.8, 50.4, 55.5, 61.2, 65.3, 70.5, 74.5
23 ])
24 V_out_k1 = np.array([
25     4.11, 4.40, 6.43, 8.53, 10.6, 12.8, 16.0, 18.8, 20.3, 22.6,
26     26.8, 33.6, 37.9, 42.2, 45.4, 49.6, 54.9, 58.7, 63.4, 67.0
27 ])
28
29 # K10 data
30 V_in_k10 = np.array([
31     4.71, 5.07, 7.41, 9.94, 12.1, 14.6, 15.3, 15.8, 16.0, 16.4,
32     18.5, 21.3, 23.3, 30.2, 40.2, 50.3, 74.5
33 ])
34 V_out_k10 = np.array([
35     41.2, 44.5, 64.5, 86.5, 105, 128, 135, 139, 141, 141,
36     141, 141, 141, 141, 141, 141, 141
37 ])
38
39 # -----
40 # Measurement uncertainty (output only)

```

```

41 # -----
42 V_out_err_k1 = np.full_like(V_out_k1, 0.1, dtype=float)
43 V_out_err_k10 = np.full_like(V_out_k10, 0.1, dtype=float)
44
45 # -----
46 # Linear range cutoff for K10
47 # -----
48 cutoff_k10 = 16.0 # linear behavior assumed for V_in <= 16.0 V
49
50 # -----
51 # Fit through origin: V_out = K * V_in
52 # with standard error from residuals
53 # -----
54 def fit_through_origin_with_error(x: np.ndarray, y: np.ndarray):
55     """
56     Least-squares fit through the origin: y = K*x
57     Returns:
58         K      : fitted slope
59         K_err   : standard error of slope from residual scatter
60         y_fit   : fitted y values
61         resid   : residuals
62     """
63     K = (x @ y) / (x @ x)
64     y_fit = K * x
65     resid = y - y_fit
66     n = len(x)
67
68     # standard error of slope for fit through origin
69     K_err = np.sqrt((resid @ resid) / ((n - 1) * (x @ x)))
70     return float(K), float(K_err), y_fit, resid
71
72 # -----
73 # Rounding helper
74 # Rule:
75 # - usually 1 significant digit in uncertainty
76 # - 2 significant digits if first digit is 1 or 2
77 # - value rounded to same decimal place as uncertainty
78 # -----
79 def round_value_uncertainty(value: float, uncertainty: float):
80     if uncertainty <= 0 or not np.isfinite(uncertainty):
81         return value, uncertainty, str(value), str(uncertainty)

```

```

82
83     exponent = int(np.floor(np.log10(abs(uncertainty))))
84     mantissa = abs(uncertainty) / (10 ** exponent)
85
86     # 2 sig figs if leading digit is 1 or 2, else 1 sig fig
87     sig_figs = 2 if mantissa < 3 else 1
88     decimals = -exponent + (sig_figs - 1)
89
90     uncertainty_rounded = round(uncertainty, decimals)
91     value_rounded = round(value, decimals)
92
93     value_str = f"{value_rounded:.{decimals}f}"
94     uncertainty_str = f"{uncertainty_rounded:.{decimals}f}"
95
96     return value_rounded, uncertainty_rounded, value_str, uncertainty_str
97
98 # -----
99 # Perform fits
100 # -----
101 K1, K1_err, _, _ = fit_through_origin_with_error(V_in_k1, V_out_k1)
102
103 mask_k10_linear = V_in_k10 <= cutoff_k10
104 K10, K10_err, _, _ = fit_through_origin_with_error(
105     V_in_k10[mask_k10_linear],
106     V_out_k10[mask_k10_linear]
107 )
108
109 # Rounded values for report output
110 K1_r, K1_err_r, K1_str, K1_err_str = round_value_uncertainty(K1, K1_err)
111 K10_r, K10_err_r, K10_str, K10_err_str = round_value_uncertainty(K10, K10_err)
112
113 # -----
114 # Print output
115 # -----
116 print("Raw fit results:")
117 print(f"K1    = {K1:.6f} pm {K1_err:.6f}")
118 print(f"K10   = {K10:.6f} pm {K10_err:.6f}")
119
120 print("\nReport-ready rounded results:")
121 print(f"K1    = {K1_str} pm {K1_err_str}")
122 print(f"K10   = {K10_str} pm {K10_err_str}")

```

```

123
124 # -----
125 # Plot
126 # -----
127 fig, ax = plt.subplots(1, 2, figsize=(12, 4.8))
128
129 # ---- K1 ----
130 ax[0].errorbar(
131     V_in_k1, V_out_k1,
132     yerr=V_out_err_k1,
133     fmt="o",
134     markersize=4,
135     markerfacecolor="white",
136     markeredgewidth=1.0,
137     capsize=3,
138     elinewidth=1.1,
139     barsabove=True,
140     zorder=3,
141     label=r"Measured data ( $\sigma_{V_{\mathrm{out}}}=0.1 \ \mathrm{V}$ )"
142 )
143
144 xline_k1 = np.linspace(0, V_in_k1.max() * 1.05, 300)
145 ax[0].plot(
146     xline_k1, K1 * xline_k1,
147     linestyle="--",
148     linewidth=1.5,
149     label=r"Fit:  $V_{\mathrm{out}} = (K1_{\mathrm{str}} \pm K1_{\mathrm{err\_str}}) \cdot V_{\mathrm{in}}$ "
150 )
151
152 ax[0].set_title(r"Rectifier $K_1$")
153 ax[0].set_xlabel(r"$V_{\mathrm{in}}$ (V)")
154 ax[0].set_ylabel(r"$V_{\mathrm{out}}$ (V)")
155 ax[0].grid(True, alpha=0.3)
156 ax[0].legend(fontsize=9)
157
158 # ---- K10 ----
159 ax[1].errorbar(
160     V_in_k10, V_out_k10,
161     yerr=V_out_err_k10,
162     fmt="o",
163     markersize=4,

```

```

164     markerfacecolor="white",
165     markeredgewidth=1.0,
166     capsize=3,
167     elinewidth=1.1,
168     barsabove=True,
169     zorder=3,
170     label=r"Measured data ( $\sigma_{V_{\mathrm{out}}}=0.1 \ \mathrm{V}$ )"
171 )
172
173 xline_k10 = np.linspace(0, cutoff_k10, 300)
174 ax[1].plot(
175     xline_k10, K10 * xline_k10,
176     linestyle="--",
177     linewidth=1.5,
178     label=rf"Fit ( $V_{\mathrm{in}} \leq \{\text{cutoff\_k10:.1f}\} \ \mathrm{V}$ ): "
179         rf" $V_{\mathrm{out}} = (\{K10\_str\} \pm \{K10\_err\_str\}) \ \mathrm{V}_{\mathrm{in}}$ "
180 )
181
182 ax[1].axvline(
183     cutoff_k10,
184     linestyle="--",
185     linewidth=1.2,
186     label=rf"Cutoff:  $V_{\mathrm{in}} = \{\text{cutoff\_k10:.1f}\} \ \mathrm{V}$ "
187 )
188
189 ax[1].set_title(r"Rectifier  $K_{10}$ ")
190 ax[1].set_xlabel(r" $V_{\mathrm{in}}$  (V)")
191 ax[1].set_ylabel(r" $V_{\mathrm{out}}$  (V)")
192 ax[1].grid(True, alpha=0.3)
193 ax[1].legend(fontsize=9)
194
195 plt.tight_layout()
196 plt.show()
197
198
199
200 # -----
201 # 5.2a) Characteristics of the Filter
202 # -----
203
204 V_in = np.array([

```

```

205     4.67, 5.05, 7.56, 10.0, 15.1, 19.9, 25.1, 30.0,
206     35.1, 39.9, 45.0, 50.2, 55.1, 60.1, 65.1, 68.9, 73.9
207 ], dtype=float)
208
209 V_out = np.array([
210     2.28, 2.51, 3.60, 4.75, 7.26, 9.51, 12.0, 14.5,
211     16.9, 19.2, 21.6, 23.9, 26.2, 28.7, 31.0, 32.8, 35.1
212 ], dtype=float)
213
214 # Measurement uncertainty (output only)
215 err_out = np.full_like(V_out, 0.1, dtype=float)
216
217 # -----
218 # Linear model
219 # -----
220 def linear_model(x, a, b):
221     return a * x + b
222
223 # -----
224 # Rounding helper
225 # Rule:
226 # - uncertainty usually 1 significant digit
227 # - use 2 significant digits if first digit is 1 or 2
228 # - value rounded to same decimal place as uncertainty
229 # -----
230 def round_value_uncertainty(value: float, uncertainty: float):
231     if uncertainty <= 0 or not np.isfinite(uncertainty):
232         return str(value), str(uncertainty)
233
234     exponent = int(np.floor(np.log10(abs(uncertainty))))
235     mantissa = abs(uncertainty) / (10 ** exponent)
236
237     sig_figs = 2 if mantissa < 3 else 1
238     decimals = -exponent + (sig_figs - 1)
239
240     value_rounded = round(value, decimals)
241     uncertainty_rounded = round(uncertainty, decimals)
242
243     value_str = f"{value_rounded:.{decimals}f}"
244     uncertainty_str = f"{uncertainty_rounded:.{decimals}f}"
245     return value_str, uncertainty_str

```



```

246
247 # -----
248 # Unweighted fit
249 # -> parameter errors come from residual scatter
250 # -----
251 popt, pcov = curve_fit(linear_model, V_in, V_out)
252 slope, intercept = popt
253 slope_err, intercept_err = np.sqrt(np.diag(pcov))
254
255 # -----
256 # Goodness of fit: R^2
257 # -----
258 V_fit = linear_model(V_in, slope, intercept)
259 ss_res = np.sum((V_out - V_fit) ** 2)
260 ss_tot = np.sum((V_out - np.mean(V_out)) ** 2)
261 R2 = 1.0 - ss_res / ss_tot
262
263 # -----
264 # Rounded values for report
265 # -----
266 slope_str, slope_err_str = round_value_uncertainty(slope, slope_err)
267 intercept_str, intercept_err_str = round_value_uncertainty(intercept,
    intercept_err)
268
269 # -----
270 # Print output
271 # -----
272 print("Raw fit results:")
273 print(f"slope      = {slope:.8f} pm {slope_err:.8f}")
274 print(f"intercept = {intercept:.8f} pm {intercept_err:.8f} V")
275 print(f"R^2        = {R2:.8f}")
276
277 print("\nReport-ready rounded results:")
278 print(f"slope      = {slope_str} pm {slope_err_str}")
279 print(f"intercept = {intercept_str} pm {intercept_err_str} V")
280 print(f"R^2        = {R2:.5f}")
281
282 print("\nSuggested equation for the report:")
283 print(
284     rf"V_out = ({slope_str} pm {slope_err_str}) V_in + "
285     rf"({intercept_str} pm {intercept_err_str}) V"

```

```

286 )
287
288 # -----
289 # Plot: V_out vs V_in with error bars
290 # -----
291 plt.figure(figsize=(7.5, 5.2))
292
293 plt.errorbar(
294     V_in,
295     V_out,
296     yerr=err_out,
297     fmt="o",
298     markersize=5,
299     markerfacecolor="white",
300     markeredgewidth=1.0,
301     capsize=3,
302     elinewidth=1.0,
303     barsabove=True,
304     zorder=3,
305     label=r"Measured data ( $\sigma_{V_{\mathrm{out}}}=0.1\,\mathrm{V}$ )"
306 )
307
308 xline = np.linspace(0, max(V_in) * 1.05, 300)
309 plt.plot(
310     xline,
311     linear_model(xline, slope, intercept),
312     linestyle="--",
313     linewidth=1.7,
314     label=(
315         rf"Linear fit:  $V_{\mathrm{out}} = ({\mathrm{slope\_str}} \pm$ 
316          ${\mathrm{slope\_err\_str}}) V_{\mathrm{in}}$ "
317         rf"$\quad + ({\mathrm{intercept\_str}} \pm
318          ${\mathrm{intercept\_err\_str}}) \,\mathrm{V}$"
319     )
320 )
321 # Optional result box inside the plot
322 summary_text = (
323     rf"$a = {\mathrm{slope\_str}} \pm {\mathrm{slope\_err\_str}}$ " "\n"
324     rf"$b = {\mathrm{intercept\_str}} \pm {\mathrm{intercept\_err\_str}} \,\mathrm{V}$ " "\n"$ 
```

```

325     rf"$R^2 = {R2:.5f}$"
326 )
327
328 plt.text(
329     0.03, 0.97, summary_text,
330     transform=plt.gca().transAxes,
331     fontsize=9,
332     verticalalignment="top",
333     bbox=dict(boxstyle="round", facecolor="white", alpha=0.9)
334 )
335
336 plt.xlabel(r"$V_{in}$ (V)")
337 plt.ylabel(r"$V_{out}$ (V)")
338 plt.title(r"Band-pass Filter: $V_{out}$ vs $V_{in}$")
339 plt.grid(True, alpha=0.3)
340 plt.legend(fontsize=9)
341 plt.tight_layout()
342 plt.show()
343
344
345
346
347 # -----
348 # Plot 2: Gain vs V_in with propagated uncertainty
349 # Assumption: only V_out has uncertainty, V_in treated as exact
350 # -----
351
352 V_in = np.array([
353     4.67, 5.05, 7.56, 10.0, 15.1, 19.9, 25.1, 30.0,
354     35.1, 39.9, 45.0, 50.2, 55.1, 60.1, 65.1, 68.9, 73.9
355 ], dtype=float)
356
357 V_out = np.array([
358     2.28, 2.51, 3.60, 4.75, 7.26, 9.51, 12.0, 14.5,
359     16.9, 19.2, 21.6, 23.9, 26.2, 28.7, 31.0, 32.8, 35.1
360 ], dtype=float)
361
362 err_out = np.full_like(V_out, 0.1, dtype=float)
363
364 # Gain and propagated uncertainty
365 gain = V_out / V_in

```

```

366 gain_error = err_out / V_in
367
368 # Optional: weighted mean gain
369 weights = 1.0 / gain_error**2
370 gain_mean = np.sum(weights * gain) / np.sum(weights)
371 gain_mean_err = np.sqrt(1.0 / np.sum(weights))
372
373 # -----
374 # Plot
375 # -----
376 plt.figure(figsize=(7.5, 5.2))
377
378 plt.errorbar(
379     V_in,
380     gain,
381     yerr=gain_error,
382     fmt="o",
383     markersize=5,
384     markerfacecolor="white",
385     markeredgewidth=1.0,
386     capsize=3,
387     elinewidth=1.0,
388     barsabove=True,
389     zorder=3,
390     label=r"Measured data ( $\sigma_{V_{\mathrm{out}}}=0.1\,\mathrm{V}$ )"
391 )
392
393 # Optional horizontal line for average gain
394 plt.axhline(
395     gain_mean,
396     linestyle="--",
397     linewidth=1.5,
398     color="tab:orange",
399     label=rf"Weighted mean:  $G = \{gain\_mean:.4f\} \pm \{gain\_mean\_err:.4f\}$ "
400 )
401
402 # Optional textbox
403 summary_text = (
404     rf"$G = \{gain\_mean:.4f\} \pm \{gain\_mean\_err:.4f\}$"
405 )
406

```

```

407 plt.text(
408     0.03, 0.97, summary_text,
409     transform=plt.gca().transAxes,
410     fontsize=9,
411     verticalalignment="top",
412     bbox=dict(boxstyle="round", facecolor="white", edgecolor="tab:orange",
413               alpha=0.9)
414 )
415 plt.xlabel(r"$V_{\mathrm{in}}$ (V)")
416 plt.ylabel(r"$V_{\mathrm{out}}/V_{\mathrm{in}}$")
417 plt.title(r"Gain vs $V_{\mathrm{in}}$")
418 plt.grid(True, alpha=0.3)
419 plt.legend(fontsize=9)
420 plt.tight_layout()
421 plt.show()
422
423
424
425
426 # -----
427 # 5.2b) Characteristics of the Filter (Resonance Curve)
428 # -----
429
430 V_in = 3.74 # V (treated as exact here)
431
432 f_khz = np.array([59.8, 70.5, 80.6, 85.1, 88.9, 91.8, 93.8, 95.9, 98.2, 100.0,
433                  105.1, 110.2])
434 V_out = np.array([0.511, 0.522, 0.526, 0.527, 0.532, 0.545, 0.552, 0.563,
435                  0.542, 0.530, 0.523, 0.522])
436 V_out_err = np.full_like(V_out, 0.010, dtype=float) # V
437
438 # -----
439 # Gain and propagated errors
440 # -----
441
442 G = V_out / V_in
443 G_err = V_out_err / V_in
444
445 G_dB = 20.0 * np.log10(G)
446 G_dB_err = (20.0 / np.log(10.0)) * (G_err / G)

```

```

445 # -----
446 # Lorentzian model in linear gain
447 #  $G(f) = y_0 + A / (1 + ((f - f_0)/\gamma)^2)$ 
448 #  $\gamma$  = HWHM, so FWHM =  $2 \cdot \gamma$ 
449 # -----
450 def lorentzian(f, A, f0, gamma, y0):
451     return y0 + A / (1.0 + ((f - f0) / gamma)**2)
452
453 # -----
454 # Rounding helper:
455 # uncertainty -> usually 1 sig fig
456 # use 2 sig figs if first digit is 1 or 2
457 # value rounded to same decimal place
458 # -----
459 def round_value_uncertainty(value: float, uncertainty: float):
460     if uncertainty <= 0 or not np.isfinite(uncertainty):
461         return str(value), str(uncertainty)
462
463     exponent = int(np.floor(np.log10(abs(uncertainty))))
464     mantissa = abs(uncertainty) / (10 ** exponent)
465
466     sig_figs = 2 if mantissa < 3 else 1
467     decimals = -exponent + (sig_figs - 1)
468
469     value_rounded = round(value, decimals)
470     uncertainty_rounded = round(uncertainty, decimals)
471
472     value_str = f"{value_rounded:.{decimals}f}"
473     uncertainty_str = f"{uncertainty_rounded:.{decimals}f}"
474     return value_str, uncertainty_str
475
476 # -----
477 # Initial guesses
478 # -----
479 idx0 = np.argmax(G)
480 f0_guess = f_khz[idx0]
481 y0_guess = np.min(G)
482 A_guess = np.max(G) - y0_guess
483 gamma_guess = 5.0 # kHz
484
485 p0 = [A_guess, f0_guess, gamma_guess, y0_guess]

```

```

486
487 bounds = (
488     [0.0, f_khz.min(), 1e-6, -np.inf],
489     [np.inf, f_khz.max(), np.inf, np.inf]
490 )
491
492 params, cov = curve_fit(
493     lorentzian,
494     f_khz,
495     G,
496     p0=p0,
497     sigma=G_err,
498     absolute_sigma=True,
499     bounds=bounds,
500     maxfev=20000
501 )
502
503 A_fit, f0_fit, gamma_fit, y0_fit = params
504 perr = np.sqrt(np.diag(cov))
505
506 # -----
507 # Derived quantities + propagated errors
508 # -----
509 # FWHM = 2*gamma
510 FWHM_khz = 2.0 * gamma_fit
511 FWHM_err = 2.0 * perr[2]
512
513 # Q = f0 / FWHM = f0 / (2*gamma)
514 Q = f0_fit / FWHM_khz
515
516 # full covariance propagation for Q(f0, gamma)
517 dQ_df0 = 1.0 / (2.0 * gamma_fit)
518 dQ_dgamma = -f0_fit / (2.0 * gamma_fit**2)
519
520 var_Q = (
521     dQ_df0**2 * cov[1, 1]
522     + dQ_dgamma**2 * cov[2, 2]
523     + 2.0 * dQ_df0 * dQ_dgamma * cov[1, 2]
524 )
525 Q_err = np.sqrt(var_Q)
526

```

```

527 # G_peak = y0 + A
528 G_peak = y0_fit + A_fit
529 var_G_peak = cov[0, 0] + cov[3, 3] + 2.0 * cov[0, 3]
530 G_peak_err = np.sqrt(var_G_peak)
531
532 # G_peak in dB
533 G_peak_dB = 20.0 * np.log10(G_peak)
534 G_peak_dB_err = (20.0 / np.log(10.0)) * (G_peak_err / G_peak)
535
536 # -----
537 # Rounded strings for report
538 # -----
539 A_str, A_err_str = round_value_uncertainty(A_fit, perr[0])
540 f0_str, f0_err_str = round_value_uncertainty(f0_fit, perr[1])
541 gamma_str, gamma_err_str = round_value_uncertainty(gamma_fit, perr[2])
542 y0_str, y0_err_str = round_value_uncertainty(y0_fit, perr[3])
543
544 FWHM_str, FWHM_err_str = round_value_uncertainty(FWHM_khz, FWHM_err)
545 Q_str, Q_err_str = round_value_uncertainty(Q, Q_err)
546 Gpeak_str, Gpeak_err_str = round_value_uncertainty(G_peak, G_peak_err)
547 Gpeak_dB_str, Gpeak_dB_err_str = round_value_uncertainty(G_peak_dB,
    G_peak_dB_err)
548
549 # -----
550 # Print output
551 # -----
552 print("Raw fit parameters:")
553 print(f"A      = {A_fit:.6f} pm {perr[0]:.6f}")
554 print(f"f0      = {f0_fit:.6f} pm {perr[1]:.6f} kHz")
555 print(f"gamma   = {gamma_fit:.6f} pm {perr[2]:.6f} kHz")
556 print(f"y0      = {y0_fit:.6f} pm {perr[3]:.6f}")
557
558 print("\nRaw derived quantities:")
559 print(f"FWHM    = {FWHM_khz:.6f} pm {FWHM_err:.6f} kHz")
560 print(f"Q       = {Q:.6f} pm {Q_err:.6f}")
561 print(f"G_max   = {G_peak:.6f} pm {G_peak_err:.6f}")
562 print(f"G_max   = {G_peak_dB:.6f} pm {G_peak_dB_err:.6f} dB")
563
564 print("\nReport-ready rounded results:")
565 print(f"f0      = ({f0_str} pm {f0_err_str}) kHz")
566 print(f"gamma   = ({gamma_str} pm {gamma_err_str}) kHz")

```



```

567 print(f"FWHM    = ({FWHM_str} pm {FWHM_err_str}) kHz")
568 print(f"Q      = {Q_str} pm {Q_err_str}")
569 print(f"G_max   = {Gpeak_str} pm {Gpeak_err_str}")
570 print(f"G_max   = ({Gpeak_dB_str} pm {Gpeak_dB_err_str}) dB")
571
572 # -----
573 # Smooth curve for plotting
574 # -----
575 f_smooth = np.linspace(f_khz.min(), f_khz.max(), 2000)
576 G_fit = lorentzian(f_smooth, *params)
577 G_fit_dB = 20.0 * np.log10(G_fit)
578
579 # -----
580 # Plot
581 # -----
582 plt.figure(figsize=(8.5, 5.5))
583
584 plt.errorbar(
585     f_khz,
586     G_dB,
587     yerr=G_dB_err,
588     fmt='o',
589     markersize=5,
590     markerfacecolor='white',
591     markeredgewidth=1.0,
592     capsize=3,
593     elinewidth=1.0,
594     barsabove=True,
595     zorder=3,
596     label=r"Measured data ( $\sigma_{V_{\mathrm{out}}}=0.010\backslash,\mathrm{V}$ )"
597 )
598
599 plt.plot(
600     f_smooth,
601     G_fit_dB,
602     linewidth=2,
603     color="tab:orange",
604     label="Lorentzian fit"
605 )
606
607 plt.axvline(

```

```

608     f0_fit,
609     linestyle="--",
610     linewidth=1.2,
611     color="tab:blue",
612     label=rf"$f_0 = ({f0_str}\pm {f0_err_str})\,,\mathrm{{kHz}}$"
613 )
614
615 summary_text = (
616     rf"$f_0 = ({f0_str}\pm {f0_err_str})\,,\mathrm{{kHz}}$" "\n"
617     rf"$\gamma = ({gamma_str}\pm {gamma_err_str})\,,\mathrm{{kHz}}$" "\n"
618     rf"$\mathrm{{FWHM}} = ({FWHM_str}\pm {FWHM_err_str})\,,\mathrm{{kHz}}$" "\n"
619     rf"$Q = {Q_str}\pm {Q_err_str}$" "\n"
620     rf"$G_{\{\max\}} = {Gpeak_str}\pm {Gpeak_err_str}$" "\n"
621     rf"$20\log_{\{10\}}(G_{\{\max\}}) = ({Gpeak_dB_str}\pm
        {Gpeak_dB_err_str})\,,\mathrm{{dB}}$"
622 )
623
624 # Summary box: upper left
625 plt.text(
626     0.03, 0.97, summary_text,
627     transform=plt.gca().transAxes,
628     fontsize=9,
629     verticalalignment='top',
630     bbox=dict(boxstyle="round", facecolor="white", alpha=0.9)
631 )
632
633 plt.xlabel("Frequency (kHz)")
634 plt.ylabel(r"Gain $20\log_{10}(G)$ (dB)")
635 plt.title("Band-pass Filter Gain (dB) with Lorentzian Fit")
636 plt.grid(True, alpha=0.3)
637
638 # Legend: lower left
639 plt.legend(
640     fontsize=9,
641     loc="lower left",
642     framealpha=0.9
643 )
644
645 plt.tight_layout()
646 plt.show()
647

```

```

648
649
650
651 # =====
652 # 5.3b) Determination of the Modulation Depth: X-Y Plot
653 # =====
654
655 # Measured values from the X-Y plot
656 A_max = 1315.0
657 A_min = 318.0
658
659 # Choose your reading uncertainties in px
660 sigma_A_max = 5.0
661 sigma_A_min = 5.0
662
663 # Modulation depth
664 m = (A_max - A_min) / (A_max + A_min)
665
666 # Error propagation
667 sigma_m = (2.0 / (A_max + A_min)**2) * np.sqrt(
668     (A_min * sigma_A_max)**2 + (A_max * sigma_A_min)**2
669 )
670
671 print(f"m = {m:.6f} pm {sigma_m:.6f}")
672
673
674
675 # -----
676 # 5.3 Modulation depth from time-domain envelope (KO method)
677 # Using full vertical heights H_max and H_min measured in pixels
678 # -----
679
680 # Measured pixel heights
681 H_min = np.array([179, 177, 182], dtype=float)
682 H_max = np.array([1135, 1136, 1130], dtype=float)
683
684 # Mean values
685 H_min_mean = np.mean(H_min)
686 H_max_mean = np.mean(H_max)
687
688 # Standard error of the mean (from 3 measurements)

```

```

689 H_min_err = np.std(H_min, ddof=1) / np.sqrt(len(H_min))
690 H_max_err = np.std(H_max, ddof=1) / np.sqrt(len(H_max))
691
692 # Modulation depth:
693 # m = (H_max - H_min) / (H_max + H_min)
694 m = (H_max_mean - H_min_mean) / (H_max_mean + H_min_mean)
695
696 # Error propagation
697 sigma_m = (2.0 / (H_max_mean + H_min_mean)**2) * np.sqrt(
698     (H_min_mean * H_max_err)**2 + (H_max_mean * H_min_err)**2
699 )
700
701 print("Measured values:")
702 print(f"H_min = {H_min_mean:.2f} pm {H_min_err:.2f} px")
703 print(f"H_max = {H_max_mean:.2f} pm {H_max_err:.2f} px")
704
705 print("\nModulation depth from KO/time-domain method:")
706 print(f"m = {m:.4f} pm {sigma_m:.4f}")
707
708
709
710 # =====
711 # 5.3 Modulation depth from FFT spectrum
712 # Semi-manual peak selection:
713 # click approximately on LSB, Carrier, USB
714 # =====
715
716 csv_path = r"C:\Users\L-Vis\OneDrive\Desktop\P3 Lab\Harmonic Analysis\USB
       Stick\5.3 total\5.3b Sinusoidal\F0002FFT.CSV"
717
718 # -----
719 # Robust CSV loader for Tektronix-like FFT exports
720 # -----
721 def load_fft_csv(path):
722     # first try normal read
723     for kwargs in [
724         dict(sep=",", engine="python"),
725         dict(sep=";", engine="python"),
726         dict(sep=None, engine="python"),
727     ]:
728         try:

```

```

729         df = pd.read_csv(path, **kwargs)
730         if df.shape[1] >= 2:
731             break
732     except Exception:
733         continue
734 else:
735     raise RuntimeError("Could not read CSV file.")
736
737 # convert all columns to numeric if possible
738 df_num = df.copy()
739 for col in df_num.columns:
740     df_num[col] = pd.to_numeric(df_num[col], errors="coerce")
741
742 valid_cols = [c for c in df_num.columns if df_num[c].notna().sum() > 5]
743
744 # fallback if headers are weird
745 if len(valid_cols) < 2:
746     raw = pd.read_csv(path, header=None, sep=None, engine="python")
747     for col in raw.columns:
748         raw[col] = pd.to_numeric(raw[col], errors="coerce")
749     valid_cols = [c for c in raw.columns if raw[c].notna().sum() > 5]
750     if len(valid_cols) < 2:
751         raise RuntimeError("Could not identify two numeric columns.")
752     df_num = raw
753
754 # choose frequency column as the one that is mostly increasing
755 freq_col = None
756 for c in valid_cols:
757     vals = df_num[c].dropna().to_numpy()
758     if len(vals) > 10:
759         frac_inc = np.mean(np.diff(vals) >= 0)
760         if frac_inc > 0.7:
761             freq_col = c
762             break
763
764 if freq_col is None:
765     # choose numeric column with most unique values
766     freq_col = max(valid_cols, key=lambda c: df_num[c].dropna().nunique())
767
768 amp_candidates = [c for c in valid_cols if c != freq_col]
769 if not amp_candidates:

```

```

770         raise RuntimeError("Could not identify amplitude column.")
771
772     amp_col = max(amp_candidates, key=lambda c: df_num[c].dropna().nunique())
773
774     out = pd.DataFrame({
775         "frequency": pd.to_numeric(df_num[freq_col], errors="coerce"),
776         "amplitude": pd.to_numeric(df_num[amp_col], errors="coerce"),
777     }).dropna()
778
779     out = out.sort_values("frequency").reset_index(drop=True)
780
781     print("Detected columns:")
782     print(f" Frequency column: {freq_col}")
783     print(f" Amplitude column: {amp_col}")
784     print(f" Number of valid rows: {len(out)}")
785
786     return out
787
788 # -----
789 # Snap click to strongest local maximum within a search window
790 # -----
791 def snap_to_local_max(f, y, x_click, window_hz=20.0):
792     mask = (f >= x_click - window_hz) & (f <= x_click + window_hz)
793     if not np.any(mask):
794         raise RuntimeError(f"No data in search window around x = {x_click:.3f}")
795
796     f_local = f[mask]
797     y_local = y[mask]
798
799     idx_local = np.argmax(y_local)
800     f_peak = f_local[idx_local]
801     y_peak = y_local[idx_local]
802
803     # map back to global index
804     global_indices = np.where(mask)[0]
805     idx_global = global_indices[idx_local]
806
807     return idx_global, f_peak, y_peak
808
809 # -----

```

```

810 # Load data
811 # -----
812 df = load_fft_csv(csv_path)
813 f = df["frequency"].to_numpy(dtype=float)
814 amp_db = df["amplitude"].to_numpy(dtype=float)
815
816 # convert dB -> linear amplitude for m calculation
817 amp_lin = 10 ** (amp_db / 20.0)
818
819 # -----
820 # First plot: user clicks 3 approximate peaks
821 # -----
822 plt.figure(figsize=(10, 5.8))
823 plt.plot(f, amp_db, linewidth=1.2)
824 plt.xlabel("Frequency")
825 plt.ylabel("Amplitude (dB)")
826 plt.title("Click approximately on: Lower sideband, Carrier, Upper sideband")
827 plt.grid(True, alpha=0.3)
828 plt.tight_layout()
829
830 print("\nPlease click on 3 peaks in this order:")
831 print("  1) lower sideband")
832 print("  2) carrier")
833 print("  3) upper sideband")
834
835 clicked = plt.ginput(3, timeout=0)
836 plt.close()
837
838 if len(clicked) != 3:
839     raise RuntimeError("You must click exactly 3 peaks.")
840
841 # search window around each click in frequency units
842 # adjust if needed
843 search_window_hz = 20.0
844
845 # snap to nearest local maximum in dB trace
846 idx_lsb, f_lsb, A_lsb_db = snap_to_local_max(f, amp_db, clicked[0][0],
847     window_hz=search_window_hz)
848 idx_car, f_c, A_c_db = snap_to_local_max(f, amp_db, clicked[1][0],
849     window_hz=search_window_hz)

```

```

848 idx_usb, f_usb, A_usb_db = snap_to_local_max(f, amp_db, clicked[2][0],
      window_hz=search_window_hz)
849
850 A_lsb = amp_lin[idx_lsb]
851 A_c    = amp_lin[idx_car]
852 A_usb = amp_lin[idx_usb]
853
854 # -----
855 # Modulation depth from spectrum
856 #  $A_{LSB} = A_{USB} = (m/2) A_C$ 
857 #  $\Rightarrow m = (A_{LSB} + A_{USB}) / A_C$ 
858 # -----
859 m_left = 2.0 * A_lsb / A_c
860 m_right = 2.0 * A_usb / A_c
861 m_avg = (A_lsb + A_usb) / A_c
862
863 # simple uncertainty estimate from sideband asymmetry
864 m_err = abs(m_left - m_right) / 2.0
865
866 # -----
867 # Print results
868 # -----
869 print("\nSelected peaks:")
870 print(f"  Lower SB: f = {f_lsb:.6g}, amplitude = {A_lsb_db:.4f} dB")
871 print(f"  Carrier : f = {f_c:.6g}, amplitude = {A_c_db:.4f} dB")
872 print(f"  Upper SB: f = {f_usb:.6g}, amplitude = {A_usb_db:.4f} dB")
873
874 print("\nConverted linear amplitudes:")
875 print(f"  A_LSB = {A_lsb:.6g}")
876 print(f"  A_C   = {A_c:.6g}")
877 print(f"  A_USB = {A_usb:.6g}")
878
879 print("\nModulation depth from spectrum:")
880 print(f"  m_left  = {m_left:.4f}")
881 print(f"  m_right = {m_right:.4f}")
882 print(f"  m_avg   = {m_avg:.4f} pm {m_err:.4f}")
883
884 # -----
885 # Final plot with selected peaks marked
886 # -----
887 plt.figure(figsize=(10, 5.8))

```



```

888 plt.plot(f, amp_db, linewidth=1.2, label="FFT spectrum")
889
890 plt.plot(f_lsb, A_lsb_db, "o", markersize=8, label="Lower sideband")
891 plt.plot(f_c, A_c_db, "o", markersize=8, label="Carrier")
892 plt.plot(f_usb, A_usb_db, "o", markersize=8, label="Upper sideband")
893
894 plt.axvline(f_lsb, linestyle="--", linewidth=1.0)
895 plt.axvline(f_c, linestyle="--", linewidth=1.0)
896 plt.axvline(f_usb, linestyle="--", linewidth=1.0)
897
898 summary = (
899     f"$f_{{\text{LSB}}} = \{f\_lsb:.3g\}$\n"
900     f"$f_C = \{f\_c:.3g\}$\n"
901     f"$f_{{\text{USB}}} = \{f\_usb:.3g\}$\n"
902     f"$m = \{m\_avg:.4f\} \backslash\text{pm} \{m\_err:.4f\}$"
903 )
904
905 plt.text(
906     0.03, 0.97, summary,
907     transform=plt.gca().transAxes,
908     fontsize=10,
909     verticalalignment="top",
910     bbox=dict(boxstyle="round", facecolor="white", alpha=0.9)
911 )
912
913 plt.xlabel("Frequency")
914 plt.ylabel("Amplitude (dB)")
915 plt.title("Modulation depth from FFT spectrum")
916 plt.grid(True, alpha=0.3)
917 plt.legend()
918 plt.tight_layout()
919 plt.show()
920
921
922
923 # =====
924 # 5.4 Finding Fourier Spectra
925 # =====
926 FOLDER = r"C:\Users\L-Vis\OneDrive\Desktop\P3 Lab\Harmonic Analysis\Harmonic
    Analysis Fourier Spectra"
927 PATTERN = "*FFT.CSV" # SinusoidalFFT.CSV, TriangularFFT.CSV, ...

```

```

928 SHOW_PLOTS = True
929 SAVE_PLOTS = True
930
931 # Zoom frs Plotten
932 XMAX_HZ = 200_000
933 N_PEAKS = 10
934
935
936 # =====
937 # Reader for TEK FFT CSV
938 # =====
939 def read_tek_fft_csv(path: str) -> tuple[np.ndarray, np.ndarray]:
940     """
941     Reads Tektronix FFT export CSV.
942     Format:
943         col 3 = Frequency [Hz]
944         col 4 = Amplitude [dB]
945     Separator is ';'
946     """
947     df = pd.read_csv(path, sep=";", header=None, engine="python")
948
949     freq = pd.to_numeric(df.iloc[:, 3], errors="coerce")
950     amp = pd.to_numeric(df.iloc[:, 4].astype(str).str.replace(",", ""),
951         regex=False),
952         errors="coerce")
953
954     mask = freq.notna() & amp.notna()
955     freq = freq[mask].to_numpy(dtype=float)
956     amp = amp[mask].to_numpy(dtype=float)
957
958     idx = np.argsort(freq)
959     return freq[idx], amp[idx]
960
961 # =====
962 # Simple peak finder
963 # =====
964 def simple_peak_list(freq: np.ndarray, amp_db: np.ndarray, n_peaks: int = 10,
965     min_freq: float = 1.0, guard_hz: float = 500.0):
966     """
967     Very simple peak finder:

```

```

968     - looks for local maxima
969     - picks top n_peaks by amplitude
970     - uses a guard band so you dont get many peaks from same bump
971     """
972     freq = np.asarray(freq)
973     amp_db = np.asarray(amp_db)
974
975     mask = (freq >= min_freq)
976     f = freq[mask]
977     a = amp_db[mask]
978
979     if len(f) < 5:
980         return []
981
982     loc = np.where((a[1:-1] > a[:-2]) & (a[1:-1] > a[2:]))[0] + 1
983     if len(loc) == 0:
984         return []
985
986     cand = loc[np.argsort(a[loc])[:, -1]]
987
988     chosen = []
989     for i in cand:
990         fi = f[i]
991         ai = a[i]
992         if all(abs(fi - fj) > guard_hz for fj, _ in chosen):
993             chosen.append((fi, ai))
994         if len(chosen) >= n_peaks:
995             break
996
997     return chosen
998
999
1000 # =====
1001 # Error estimation helpers
1002 # =====
1003 def estimate_fft_binwidth(freq: np.ndarray) -> float:
1004     """Median FFT frequency spacing."""
1005     return float(np.median(np.diff(freq)))
1006
1007
1008 def characterize_peak(freq: np.ndarray, amp_db: np.ndarray, f_guess: float):

```

```

1009     """
1010     Characterize a peak near frequency f_guess.
1011
1012     Returns:
1013         f_peak, A_peak, sigma_f, sigma_A, idx
1014     where
1015         sigma_f ~ half FFT bin width
1016         sigma_A ~ half max difference to neighboring bins
1017     """
1018     idx = int(np.argmin(np.abs(freq - f_guess)))
1019
1020     f_peak = float(freq[idx])
1021     A_peak = float(amp_db[idx])
1022
1023     # frequency uncertainty from FFT bin width
1024     df = estimate_fft_binwidth(freq)
1025     sigma_f = df / 2.0
1026
1027     # amplitude uncertainty from local bin-to-bin variation
1028     diffs = []
1029     if idx > 0:
1030         diffs.append(abs(amp_db[idx] - amp_db[idx - 1]))
1031     if idx < len(amp_db) - 1:
1032         diffs.append(abs(amp_db[idx] - amp_db[idx + 1]))
1033
1034     sigma_A = max(diffs) / 2.0 if diffs else np.nan
1035
1036     return f_peak, A_peak, sigma_f, sigma_A, idx
1037
1038
1039 def round_value_uncertainty(value: float, uncertainty: float):
1040     """
1041     Round value and uncertainty:
1042     - uncertainty: 1 sig fig usually
1043     - 2 sig figs if leading digit is 1 or 2
1044     - value rounded to same decimal place
1045     """
1046     if uncertainty <= 0 or not np.isfinite(uncertainty):
1047         return str(value), str(uncertainty)
1048
1049     exponent = int(np.floor(np.log10(abs(uncertainty))))

```

```

1050     mantissa = abs(uncertainty) / (10 ** exponent)
1051
1052     sig_figs = 2 if mantissa < 3 else 1
1053     decimals = -exponent + (sig_figs - 1)
1054
1055     value_rounded = round(value, decimals)
1056     uncertainty_rounded = round(uncertainty, decimals)
1057
1058     value_str = f"{value_rounded:.{decimals}f}"
1059     uncertainty_str = f"{uncertainty_rounded:.{decimals}f}"
1060     return value_str, uncertainty_str
1061
1062
1063 # =====
1064 # Main analysis loop
1065 # =====
1066 for path in glob.glob(os.path.join(FOLDER, PATTERN)):
1067     name = os.path.basename(path)
1068
1069     freq, amp_db = read_tek_fft_csv(path)
1070
1071     # Find candidate peaks
1072     peaks = simple_peak_list(
1073         freq,
1074         amp_db,
1075         n_peaks=N_PEAKS,
1076         min_freq=1.0,
1077         guard_hz=500.0
1078     )
1079
1080     if len(peaks) == 0:
1081         print(f"\n{name}: no peaks found.")
1082         continue
1083
1084     # Fundamental = strongest non-DC peak
1085     f1_guess, A1_guess = max(peaks, key=lambda x: x[1])
1086
1087     # Third harmonic = candidate closest to 3*f1
1088     peaks_no_f1 = [p for p in peaks if abs(p[0] - f1_guess) > 100.0]
1089     if len(peaks_no_f1) > 0:

```

```

1090     f3_guess, A3_guess = min(peaks_no_f1, key=lambda x: abs(x[0] - 3.0 *
1091     f1_guess))
1092     f3, A3, sf3, sA3, idx3 = characterize_peak(freq, amp_db, f3_guess)
1093     else:
1094         f3 = A3 = sf3 = sA3 = np.nan
1095         idx3 = None
1096
1097     # Refine fundamental
1098     f1, A1, sf1, sA1, idx1 = characterize_peak(freq, amp_db, f1_guess)
1099
1100     # Rounded strings
1101     f1_khz_str, sf1_khz_str = round_value_uncertainty(f1 / 1000.0, sf1 /
1102     1000.0)
1103     A1_str, sA1_str = round_value_uncertainty(A1, sA1)
1104
1105     if np.isfinite(f3):
1106         f3_khz_str, sf3_khz_str = round_value_uncertainty(f3 / 1000.0, sf3 /
1107         1000.0)
1108         A3_str, sA3_str = round_value_uncertainty(A3, sA3)
1109
1110     # =====
1111     # Console output
1112     # =====
1113     print("\n" + "=" * 70)
1114     print(f"File: {name}")
1115     print("=" * 70)
1116
1117     print("\nRaw peak values:")
1118     print(f"f1 = {f1:.3f} pm {sf1:.3f} Hz")
1119     print(f"A1 = {A1:.3f} pm {sA1:.3f} dB")
1120
1121     if np.isfinite(f3):
1122         print(f"f3 = {f3:.3f} pm {sf3:.3f} Hz")
1123         print(f"A3 = {A3:.3f} pm {sA3:.3f} dB")
1124
1125     print("\nReport-ready rounded values:")
1126     print(f"f1 = ({f1_khz_str} pm {sf1_khz_str}) kHz")
1127     print(f"A1 = ({A1_str} pm {sA1_str}) dB")
1128
1129     if np.isfinite(f3):
1130         print(f"f3 = ({f3_khz_str} pm {sf3_khz_str}) kHz")

```

```

1128     print(f"A3 = ({A3_str} pm {sA3_str}) dB")
1129     print(f"Check: f3 / f1 = {f3/f1:.3f}")
1130
1131     # =====
1132     # Plot (unchanged style)
1133     # =====
1134     if SHOW_PLOTS or SAVE_PLOTS:
1135         plt.figure(figsize=(9, 4.8))
1136         plt.plot(freq, amp_db, linewidth=0.8)
1137         plt.xlim(0, XMAX_HZ)
1138         plt.xlabel("Frequency [Hz]")
1139         plt.ylabel("Amplitude [dB]")
1140         plt.title(f"FFT spectrum (exported) - {name}")
1141         plt.grid(True, alpha=0.3)
1142
1143         if idx1 is not None:
1144             plt.plot(freq[idx1], amp_db[idx1], "o", markersize=5)
1145
1146         if idx3 is not None:
1147             plt.plot(freq[idx3], amp_db[idx3], "o", markersize=5)
1148
1149         plt.tight_layout()
1150
1151         if SAVE_PLOTS:
1152             out_png = os.path.splitext(path)[0] + ".png"
1153             plt.savefig(out_png, dpi=300)
1154
1155         if SHOW_PLOTS:
1156             plt.show()
1157         else:
1158             plt.close()
1159
1160
1161
1162     # =====
1163     # Main
1164     # =====
1165     files = sorted(glob.glob(os.path.join(FOLDER, PATTERN)))
1166     if not files:
1167         raise FileNotFoundError(f"No files matching {PATTERN} in {FOLDER}")
1168

```

```
1169 for path in files:
1170     name = os.path.basename(path)
1171     freq, amp_db = read_tek_fft_csv(path)
1172
1173     # Peaks (for report table)
1174     peaks = simple_peak_list(freq, amp_db, n_peaks=N_PEAKS)
1175
1176     print("\n" + "=" * 70)
1177     print("File:", name)
1178     print(f"Freq range: {freq.min():.1f} .. {freq.max():.1f} Hz")
1179     print("Top peaks (freq [Hz], amp [dB]):")
1180     for f0, a0 in peaks:
1181         print(f"  {f0:12.2f}  {a0:8.2f}")
1182
1183     # Plot
1184     plt.figure(figsize=(10, 5))
1185     plt.plot(freq, amp_db, linewidth=1)
1186     plt.xlabel("Frequency [Hz]")
1187     plt.ylabel("Amplitude [dB]")
1188     plt.title(f"FFT spectrum (exported) - {name}")
1189     plt.grid(True)
1190     plt.xlim(0, XMAX_HZ)
1191     plt.tight_layout()
1192
1193     if SAVE_PLOTS:
1194         out_png = os.path.splitext(path)[0] + "_clean.png"
1195         plt.savefig(out_png, dpi=200)
1196         print("Saved plot:", out_png)
1197
1198     if SHOW_PLOTS:
1199         plt.show()
1200     else:
1201         plt.close()
```